

APPENDIX A Chemical methods for predicting the acid mine drainage/acid rock drainage potential of mine wastes in Australia

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Introduction

Prediction techniques for acid mine drainage/acid rock drainage (AMD/ARD) provide the foundation for developing control and management plans for mine wastes by assisting in the prevention or mitigation of the environmental impact arising from the oxidation of sulphidic mine wastes. The objectives of predictive tests are to (a) determine if a discrete volume of mining waste will generate acid and (b) to predict the drainage quality based on the measured rate of acid formation. Prediction methods can apply to both individual material types or the entire waste dump, although the latter is an extremely complex task.

A complete predictive assessment requires understanding of a number of factors including the nature of the deposit, the mineralogy, the mining and processing operations in addition to local environment and climatic factors. The components affecting the total capacity of a mining waste to generate acid are characterised by the amount of acid generating minerals present (generally sulphides), and the amount of neutralising minerals present. The rate of acid generation is influenced by the type of sulphide mineral, the type of carbonate and other neutralising minerals, the mineral surface area available for reaction, the availability of water and oxygen and the presence of bacteria.

Chemical prediction tests in AMD/ARD fall into two categories, namely static tests and kinetic tests. These have been the subject of a number of comprehensive reviews overseas (BC Task Force 1989, Coastech 1989, USEPA 1994).

Static tests

A static test determines both the total acid generating and total acid neutralising potential of a sample and is used to predict the potential to produce acid. The standard convention adopted in Australia and the Asia Pacific region is to express the potential for a sample to generate or consume acid in terms of kg H₂SO₄ equivalence per tonne of waste. This differs from the convention adopted in the United States and Canada where the potential for a sample to generate or consume acid is in terms of kg CaCO₃ equivalence per tonne of waste. The capacity of the sample to generate acidic drainage is calculated as either the difference between, or ratio of, values of acid and neutralisation potentials. Classification schemes are then used to classify the materials as acid generating, non-acid generating or potentially acid generating.

Static tests are conducted quickly and are relatively inexpensive to undertake relative to total mining costs. There are a number of variations of static tests available to predict the acid generation potential of mine wastes as summarised in table A1. Acid-base accounting tests (ABA), modified acid-base accounting tests, BC Research Initial test and the alkaline production test evaluate a maximum potential acidity (MPA) or acid potential (AP), in addition to a neutralisation potential (NP) or acid neutralising capacity (ANC). Variations in the estimation of the acid neutralising capacity via these different methods have resulted in a difference of opinion as to the 'most appropriate' or 'correct' methods, and are often the subject of debate in the AMD/ARD arena (Lapakko 1994, Calow et al 1995).

The hydrogen peroxide test, net acid production test and net acid generation test involve reacting the sample with a strong oxidant, namely hydrogen peroxide, evaluating the net acid production without measuring the acid generation and neutralising potentials separately.

Table A1 Summary of static testwork in AMD/ARD prediction

Static test	Method	Reference
Acid base accounting	The acid potential is based on total S or sulphide S. The neutralisation potential is determined by reacting a finely ground sample with excess HCl as indicated by the Fizz test. The mixture is heated, cooled and titrated to pH 7.0.	Sobek et al 1978
Modified acid base accounting	The acid potential is based on sulphide S. The neutralisation potential is estimated by reacting a finely ground sample with excess HCl as indicated by the Fizz test. The sample is agitated at room temperature for 23 h, followed by titration to pH 8.3.	Coastech 1989
BC Research Initial	The acid potential is based on total S. The neutralisation potential is determined by titration of the finely ground sample as a slurry to pH 3.5 with 1 normal H_2SO_4 .	Duncan & Bruynesteyn 1979
Alkaline production: sulphur	The neutralisation potential is determined by reacting 20 mL 0.1 molar HCl with 0.4 g solid for 2 h at room temperature followed by titration to pH 4.0.	Caruccio et al 1981
Hydrogen peroxide test	The amount of pyrite in the sample is determined by comparing rates of oxidation with peroxide and comparing temperature profiles against pyrite standards.	Finkelman & Giffin 1986
Modified hydrogen peroxide test	Alkaline components are removed with 6 molar HCl prior to oxidation reaction with hydrogen peroxide.	O'Shay et al 1990
Net acid production	Reaction with hydrogen peroxide followed by titration to pH 7.0.	Coastech 1989
Net acid generation	250 mL 15% peroxide to 2.5 g sample. React at room temperature for several hours. Titrate to pH 7.0 if final NAG pH is less than 4.0. Temperature profiles may also be measured.	Miller et al 1991

Kinetic tests

Static prediction techniques are useful screening tools for broadly classifying mine wastes. However, they give no information on time-related reaction kinetics nor predict the short and long-term drainage water quality in the field. Such information is obtained by kinetic tests. The tests may be performed in the laboratory and are of a longer duration than static tests and are considerably more expensive to undertake. However, such tests provide information on the rate of sulphide oxidation, rate of acid generation, rate of neutralisation and the nature of pollutants that may be leached out from the materials under certain conditions. Kinetic tests may also be used to test control measures for the wastes (such as layering and blending) and are also used to simulate processes occurring at mining sites.

There are a number of kinetic acid mine drainage prediction techniques that have been utilised over the last two decades. These include humidity cells, humidity columns, the BC Research Confirmation test, batch reactor tests, soxhlet reactor tests, column tests and field tests. Table A2 briefly outlines the nature of these tests. The most commonly used kinetic tests are humidity cells and column tests. Data from both static and kinetic tests used in characterising mine waste samples from various mine sites around the world is currently being collected and collated for an international kinetic database (Ferguson & Morin 1991; Morin 1996).

Table A2 Summary of kinetic tests in AMD/ARD prediction

Kinetic test	Method	Reference
Humidity cells	200 g of crushed rock (-2 mm particle size) exposed to 3 days dry air, 3 days humidified air and rinsed with 200 mL of distilled water on the seventh day. Leachate analysed for a number of parameters. Test run for 20 or more weeks.	Sobek et al 1978
Humidity columns	50 to 60 kg of coarse rock material. Water flushing rate equivalent to specific site rainfall. Weekly volume added over 5 days as slow continuous trickle with 50% added on last day. Continuous air flushing through cell. Leachate analysed for a number of parameters. Tests run for minimum of 20 weeks.	Brodie et al 1991
BC Research Confirmation	5–30 g (-400 mesh particle size) added to bacterially active solution at pH 2.3 to 2.5 and temperature of 35°C.	Duncan & Bruynesteyn 1979
Column tests	Columns containing mine wastes are leached with discrete volumes of water for minimum of 20 weeks. Leachates analysed for a number of parameters.	Bruynesteyn & Hackl 1982; Hood & Oertel 1984; Ferguson & Morin 1991; Miller et al 1995
	Many variations to basic column leach test include wet/dry cycles, flushing rates, water application rates, recirculation or single pass, inoculation with bacteria, etc.	
Batch reactor tests/shake flask tests	200 g of sample (-200 mesh particle size) is agitated in 500 mL of distilled water as a slurry.	Halbert et al 1983.
Soxhlet extraction test	Sample is leached with hot distilled water using soxhlet apparatus for several days to several weeks. The leachates are monitored for a number of parameters.	Sullivan & Sobek 1982
Modified NAG tests	Samples reacted with peroxide. Temperature and pH profiles monitored.	Miller & Jeffrey 1995
Field tests	Test piles constructed on liners using field scale particles. Flow and water quality data collected.	Edgar & Lapakko 1985

Sampling

Sampling is one of the most critical aspects of any prediction program. As the purpose of testing rock material is to allow classification and planning of waste disposal, samples must be selected to characterise both the type and volume of rock materials and also account for the variability of materials that will be exposed during mining. The representativeness of the sample is also a critical part of the assessment program and the number of samples should cover the boundaries of variability within geological units. In addition, the method of sample collection, the length of time of storage and the sample storage environment are important factors for consideration prior to testwork. This subject has been considered in detail in a study undertaken for the Mine Environment Neutral Drainage (MEND) Program in Canada in 1992 (SENES 1992).

The USEPA has also summarised a number of options concerning the number of samples to be collected in a fixed frequency sampling program. The procedural steps recommended in predicting the acid generating potential of mine wastes have been summarised in a recent review as follows (USEPA 1994):

1. Define the geological (or lithological) units that will be encountered during mining. Describe the geology and mineralogy of these units in detail.
2. Develop a sampling plan based on an understanding of geology (eg rock mass, etc). Collect samples to represent a range of compositional variation within a rock unit.
3. Select static or kinetic tests and evaluate potential for acid formation.

4. Evaluate sampling criteria and conduct additional kinetic tests as required.
5. Develop a model as appropriate.
6. Based on findings, classify geological (lithological) units as acid generating, non-acid generating or uncertain.

The responses pertaining to waste characterisation from the OSS/ACMRR questionnaire suggest that the Australian mining industry needs to adopt similar procedural steps to ensure standardisation and uniformity in AMD/ARD prediction.

Review of chemical prediction methods currently used in Australia

This section reviews both static and kinetic methods and classification schemes generally used in Australia for assessing the AMD/ARD potential of mine wastes. The methods reviewed are specifically acid base accounting (ABA), the net acid generation (NAG) test, the kinetic NAG tests, the geochemical abundance index (GAI) and leach column testwork. Limitations that may be associated with each method are highlighted where appropriate. The criteria for classifying mine wastes as used within the Australian mining industry will also be discussed. On-site water quality monitoring, predictive modelling and field determination of the intrinsic oxidation rate (IOR) will only be briefly described in the present review.

Acid-base accounting methodology

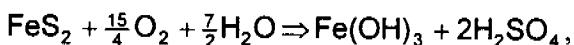
Acid-base accounting methodology includes measurement of pH and salinity of a paste of the waste material, a measurement of the acid potential (AP) and the acid neutralising capacity (ANC).

pH and salinity of the saturated paste

The pH measurements of the saturated paste provide an indication of the inherent acidity (or alkalinity) of the material. The pH measurement does not predict the acid-forming potential of the material but reflects the *in-situ* pH of the sample, indicating the immediate reactivity of sulphides and acid neutralising minerals within the sample. The pH of the saturated pastes have generally been determined at sample/water ratios of 1:1, 1:2, 1:2.5 and/or 1:5, the higher dilutions generally used to minimise glass electrode deterioration and to provide supernatant for electrical conductivity measurements. Electrical conductivity (EC) measurements of the saturated paste provide an indication of the salinity of the material. The EC provides an indirect measure of the amount of water soluble salts in the sample. The EC of a 1:5 sample/water extract is generally determined according to an APHA method (Rayment & Higginson 1992).

Acid potential, AP or maximum potential acidity (MPA)

The acid potential (AP), also termed the maximum potential acidity (MPA), is a function of the total %S in the material and is calculated based on the reaction stoichiometry for pyrite oxidation. This assumes that all sulphur is present as reactive pyrite, and further, that the reaction proceeds to completion. Based on the following stoichiometry for pyrite oxidation,



the maximum acidity produced by a sample containing 1% S as pyrite is 30.6 kg H₂SO₄/t.

The use of the pyritic sulphur content of a material gives a better estimate of the acid potential, but also increases analytical costs. Often, the sulphidic sulphur content is determined as the difference between the total sulphur content and the sulphate sulphur content, and this is used for the theoretical estimate of the acid potential. However, to

accurately estimate the acid potential of the material, it is important to indicate the type of sulphur used in the calculation, and to understand the behaviour of the forms of sulphur in the mine waste.

Methods that assume that sulphur present as sulphate is not acid producing may lead to an underestimate of the acid potential if jarosites and/or other acid producing sulphates are present. In addition, other acid generating sulphides have different stoichiometries from pyrite and need to be accounted for in the theoretical calculation of the acid potential. Nevertheless, there may be non-acid generating sulphates and/or organic sulphur as well as non-acid producing sulphides present. These latter minerals do not contribute to the acid potential but, if present, may cause gross overestimation of the acid potential if the total sulphur content is used for the theoretical estimation of the maximum acid potential.

Acid neutralising capacity (ANC)

Acid formed from pyrite oxidation may react with gangue minerals in the rock and this is quantified in terms of the acid neutralising capacity (ANC). The minerals which contribute most to the overall acid neutralising capacity are usually carbonates such as calcite and dolomite.

The acid neutralising capacity of a waste can be estimated in a number of ways. Generally, it is determined by reacting a sample with a known amount of standardised hydrochloric acid, heating this solution to enhance reaction, and back titrating to determine the amount of acid consumed (Sobek et al 1978). The amount of acid consumed during the test represents the inherent acid neutralising capacity of the sample and is expressed in units of kg H₂SO₄ per tonne of material. A number of limitations are associated with this experimental method. Firstly, hydrochloric acid is not the acid generated in the field, and, additionally, the use of strong acid concentrations may dissolve minerals that may not necessarily dissolve under field conditions. Secondly, neutralisation does not take place at, or close to, boiling and the use of boiling acid for those tests may cause overestimation of the ANC by reacting with iron and manganese carbonates.

The modified acid base accounting method replaces the heating process with agitation of the sample with acid for 24 h at room temperature (Coastech 1989). In this case, the ANC may be underestimated as some acid consuming minerals react very slowly in cold hydrochloric acid. Nevertheless, both methods are widely used in the mining industry in Australia due to the low cost of the test and the short time required to complete the test, allowing for analysis of many samples in a short time frame.

Associated with the acid base accounting method is the Fizz test which is a simple test in which the carbonate content of a sample is estimated by observing the intensity of the reaction between a small quantity of the sample and strong hydrochloric acid (Sobek et al 1978). The presence of calcium carbonate is indicated by bubbling or an audible 'fizz'. This fizz is rated on a scale of 0 to 3 from no reaction to a strong reaction and is used to determine the volume and normality of HCl required in ABA testwork. Naturally, there is some degree of subjectivity in determining the fizz rating.

Another method for determining the ANC involves the slow titration of the material with either standardised hydrochloric or sulphuric acid usually to a pH of 3.5. While this titration method may allow for pH values closer to those observed in the field, as opposed to the low pH used in the back titration of the ABA method, there is the possibility of complexation and common ion effects, which may impact on the ANC determination. In addition, some acid consuming minerals react slowly with weak sulphuric acid. The method also requires the use

of sophisticated equipment such as automatic titrators, and is time consuming relative to the back titration method, requiring times of at least 24 hours for completion rather than the several hours required for the back titration method. It is not known whether this former method is widely utilised in Australia, but it has been used overseas (Calow et al 1995).

A simple and relatively cheap method of estimating the ANC is based on the total carbon content of the mine waste sample. This method has found usage in some mines in Australia and requires calibration and validation for each specific site. The method would probably not be suitable for coal mines which contain a high abundance of organic carbon.

It is important to ensure a satisfactory determination of the neutralisation potential since its value will impact on the classification of mine wastes as acid generating or non-acid generating. Erroneous classification of an acid generating waste as non-acid generating may result in unanticipated environmental liability.

Net acid producing potential (NAPP)

The net acid producing potential (NAPP) is the theoretical balance between the sample's capacity to generate acid (via the oxidation of sulphides) and its capacity to neutralise any acid liberated (ie ANC). The classification of mine wastes as acid generating or non-acid generating is based on NAPP values and will be discussed in detail below.

The net acid generation (NAG) test

The NAG test provides a measure of the net amount of acid remaining in a sample after all the acid generating and acid neutralising reactions have taken place. In effect, it provides a direct assessment of the potential for a material to produce acid after a period of exposure and weathering. The method uses hydrogen peroxide to oxidise the sulphides contained in the waste. All, or part, of the acid generated by this oxidation is then consumed by the base materials that may be present. A NAG final pH less than 4 would confirm that the material has the potential to generate acid after a period of exposure to oxidising conditions in the field. The net amount of acid remaining after the NAG reaction is determined by titration to pH 7.0. In this case, the NAG is expressed as kg H₂SO₄ produced per tonne of material.

The NAG test has been developed as an appropriate field test by Environmental Geochemistry International Pty Ltd (EGI) with funding by members of the Australian Mineral Industries Research Association Pty Ltd (AMIRA) (Miller & Jeffery 1995). AMIRA commissioned EGI to carry out a detailed investigation of the NAG test in 1994 to investigate its potential as a reliable tool for field use within the Australian mining industry. The results of the study generally confirmed the suitability of the NAG test as a reliable tool for predicting the acid generating potential of mine wastes, and for reducing the uncertainties associated with the NAPP prediction procedure from acid-base accounting. However, the study showed that it is important to carry out both NAPP and NAG tests on a sufficiently large number of samples to calibrate the NAG test for routine use at any one particular site. This is particularly important for coal deposits where the organic materials present may preferentially react with the peroxide and for sites where the presence of copper oxide and/or manganese dioxide could catalyse peroxide decomposition.

The kinetic net acid generation (kinetic NAG) test

Kinetic NAG tests involve the continual monitoring of pH and temperature trends after peroxide addition. These tests may vary widely between material types as a function of the inherent oxidation, acid generation and acid neutralisation characteristics of the material. An objective of the above AMIRA research program was to determine if the kinetics of the NAG test reaction could be related to real-time kinetics of sulphide oxidation and acid generation.

A relationship has been observed between NAG reaction kinetics and the lag period in leach columns before the columns go acid. Work is continuing in this area so that the relationship between the kinetic NAG test, column leach test results and field behaviour is further developed (Miller 1996).

Criteria for classifying mine wastes

Two criteria commonly used internationally for categorising mine waste samples are the net acid producing potential (NAPP) and the acid potential ratio (APR). The NAPP has the greatest usage in Australia whilst the APR is slowly being adopted by some mines. It is recommended that both criteria are used in conjunction to more accurately classify mine wastes. The NAPP and APR are derived from acid base accounting data.

Net acid producing potential (NAPP)

The NAPP is calculated from the following equation:

$$\text{NAPP (kg H}_2\text{SO}_4/\text{tonne}) = 30.6 \text{ S (\%)} - \text{ANC (kg H}_2\text{SO}_4/\text{tonne})$$

The calculation assumes that all sulphur is present as 'oxidisable' sulphide, and that all ANC is available for reaction with acid generated by sulphide oxidation. Theoretically, a sample with $\text{NAPP} > 0$ is classified as potentially acid generating and a sample with $\text{NAPP} \leq 0$ is classified as non-acid generating. However, this simple classification does not take into account the capacity, or risk, that a sample may generate acid, nor does it provide any indication of the exposure time necessary before the onset of acid conditions. Nevertheless, for NAPP values greater than 20 kg H₂SO₄/tonne and less than -20 kg H₂SO₄/tonne, the NAPP classification has general reliability (Hutchison & Ellison 1992). For samples in the range -20 to +20 kg H₂SO₄/tonne, there is some degree of uncertainty due to issues such as sulphide reactivity, and the nature and availability of ANC and kinetic processes.

Acid potential ratio

The acid potential ratio is the ratio of neutralising potential (ANC) to acid potential (AP) of the sample. A sample with ANC/AP less than unity is classified as potentially acid generating whilst a sample with ANC/AP greater than 3 is non-acid generating. A zone of uncertainty remains for values between unity and 3 (Hutchison & Ellison 1992).

The NAG test criteria

The NAG test was initially introduced as a confirmatory test for classifying mine wastes into the various categories, thereby reducing the uncertainties associated with the NAPP procedure. Where discrepancies are noted between NAPP and NAG tests, further investigations are warranted on the material. Miller (1996) has defined four main categories based principally on the NAPP and static NAG test results for classification of mining wastes. These categories are specifically: acid consuming materials (ACM), non-acid generating (NAF), potentially acid generating-low capacity (PAF-LC) and potentially acid generating-high capacity (PAF-HC). The criteria for these categories are summarised in table A3.

The geochemical abundance index (GAI)

The geochemical abundance index (GAI) has been used by some sites in Australia to assess the extent of elemental enrichment in mine waste samples. The GAI quantifies an assay result for a particular element in terms of the average crustal abundance for that element (Miller 1995). The index, based on a log 2 scale, is expressed in 7 integer increments (0 to 6). As a general rule, a GAI greater than 3 indicates enrichment to a level that warrants further investigations. Any elevated element level can be compared with published soil/waste criteria

(ANZECC 1992). Values above the published criteria indicate a need to assess the degree of mobility, reactive state and sensitivity to the potential receiving environment.

The overall purpose of the GAI is to identify metals that occur at concentrations which are well above normal background levels. Naturally, in a mineralised deposit, this is likely to be the case and it should be pointed out that the GAI itself does not assess the mobility or reactivity of metals. This can only be determined by further tests such as column leach tests.

Table A3 Classification of mine wastes according to Miller (Miller 1996)

Category	Criteria
Acid consuming material (ACM)	ANC/MPA > 3; ANC in the order of 50 kg H ₂ SO ₄ /t and sulphide S content less than 0.5% S.
Non-acid generating (NAF)	NAG pH greater than 4; negative NAPP values
Potentially acid generating – low capacity (PAF-LC)	NAG pH less than 4; NAG values less than about 5 to 10 kg H ₂ SO ₄ /t after titration to pH 7; positive NAPP values
Potentially acid generating – high capacity (PAF-HC)	NAG pH less than 4; NAG values greater than 10 kg H ₂ SO ₄ /t after titration to pH 7; positive NAPP values.

Leach column testwork

Geochemical kinetic tests, particularly column tests, are used to determine relative rates of acid generation, neutralisation and metal depletion; to compare leaching behaviour of different mine rock classes and types; predict drainage water quality; select or confirm mine rock management and control options; represent site conditions to determine factors controlling AMD; and/or to produce raw data for modelling of environmental impact.

In column testwork, water is added to a sample, the mixture is allowed to incubate for a certain period of time, and samples of leachates are collected and analysed. A number of water application methods are possible including flooding, trickling, continuous application or intermittent application. The leachates are collected periodically and analysed for water quality parameters such as pH; conductivity; acidity or alkalinity; sulphate concentration; calcium and magnesium concentration and dissolved metals. The pH of the collected leachate helps to identify the stage of the acid drainage process. The sulphate production is related to the rate of acid generation and can be used to estimate the intrinsic oxidation rate (IOR) of the material provided sulphate is conserved. The IOR will be discussed in detail below. The calcium and magnesium concentrations can be related to the rate of neutralisation. Additionally, the acidity or alkalinity gives an indication of the extent of acid production or acid neutralisation.

Once the rate of sulphide oxidation is deduced, an estimate can be made of the rate of sulphide depletion and the time to oxidise all the sulphide present in the column, based on the sulphide content of the material. Similarly, an estimate can be made of the rate of depletion of neutralisation potential and the time to consume carbonates present in the waste. These estimates are based on simplistic assumptions that the dominant processes occurring are oxidation by pyrite and neutralisation by calcite.

Column tests can take a long time to provide meaningful results and it is important to ensure they are operated under expected field conditions of wetting and drying. Additionally, the interpretation of test results is site specific and requires careful consideration of climatic factors. There is no standard protocol for column testwork within the Australian mining

industry (nor internationally) and only two examples are given below to highlight some of the variations in the methodology.

At the Australian Nuclear Science and Technology Organisation (ANSTO), a typical leaching apparatus comprises a 30 cm diameter PVC column and contains up to 20 kg of mine waste material. The material to be leached is contained in this vessel with no specific compaction technique. Waste rocks are crushed to a nominal size of less than 2 cm, using a rule of thumb that the largest particle in the column should be less than 10% of the column diameter to minimise edge effects, whilst tailings are leached as received. Deionised water is slowly and uniformly dispersed over the entire surface area to ensure complete wetting of the sample. The geometry of the leaching apparatus and the volume of deionised water delivered is selected to closely simulate the average annual rainfall at the mine site as well as to provide sufficient volume of leachate for analysis. The columns are irrigated weekly as a single rainfall event and a heat lamp is situated directly above the column to heat the surface of the columns for eight hours a day, simulating insolation.

The standard column set up used by EGI involves sample sizes of 2.5 kg, crushed to a nominal 4 mm size for waste rock, or used as received for tailings. The sample is placed in the column and initially leached with deionised water at a rate of 400 mL/kg. Leaching with deionised water is carried out at a rate of 100 mL/kg for three weeks and 400 mL/kg for the fourth week. The leachate is collected subsequent to the fourth week's addition and analysed for a number of water quality parameters. The columns are exposed to drying conditions between water additions via the use of heat lamps (Miller & Jeffery 1995).

On-site water quality monitoring

A number of respondents to the OSS/ACMRR survey indicated that they monitored pH as part of their on-going water quality monitoring. Such measurements provide an indication of the parameters that should be analysed and monitored over time (Miller 1995). Early indicators of sulphide oxidation in mine site drainage are increasing sulphate concentrations, increasing concentrations of major cations and a shift in pH. The chemical composition of AMD/ARD is very much dependent on the mineralogy of the waste material. Metals that should be monitored include Mn, Zn, Cu, Al and Fe. Other metals that should be included depend on their level of enrichment in the sample relative to acceptance criteria for assessing soil toxicity. These elements will be of concern if they are soluble and leach into the environment. Alkalinity is also an important parameter to measure since it will indicate the presence of carbonates.

Predictive modelling

In a recent Minerals Council of Australia environmental workshop, Woodward-Clyde presented information on preliminary waste block models presently in construction for some recently proposed developed mine sites in Australia (Scott et al 1996). The testwork programs at these sites have been specifically designed to identify the temporal selective handling requirements for AMD prevention during the mining operation. Sampling has involved collection of representative combinations of all waste types identified within the geological database and samples have been subjected to static, kinetic and accelerated predictive tests to build up a database for construction of the preliminary waste block model.

There is also potential for kinetic models to be applied to Australian mine sites to estimate the production of contaminants arising from AMD/ARD. In kinetic modelling, a steady-state geochemical model is constructed to study the water-rock interactions controlling metal release from a waste rock heap. The waste rock heap is treated as a single completely mixed

flow-through reactor of unit cross-sectional area and specified height. The geochemical model may include kinetics of sulphide and primary silicate weathering, aqueous speciation equilibrium, formation of secondary mineral phases, and transport. From the joint use of kinetic and geochemical modelling, estimates of the quality of drainage from waste rock piles can be obtained. These tools could be instrumental in providing useful information and predictions that could be adopted in mine planning strategies and rehabilitation measures for waste rock dumps.

ANSTO has used both geochemical and kinetic modelling as a first estimate of the release of hazardous material from two uranium mines in Germany (Brown & Lowson 1997). The potential for release of hazardous materials from these sites was controlled by carbonate and sulphide minerals. The models were based on a steady-state geochemical model developed by Stromberg and Banwart (1994) to study water–rock interactions controlling metal release from waste rock heaps at a copper mine in northern Sweden, and STEADYQL, a mathematical model developed by Furrer et al (1989, 1990) for studying the composition and speciation of soil solutions. For both the copper mine in Sweden and the uranium mines in Germany, field monitoring of drainage water composition has provided a basis for evaluation of model performance.

The intrinsic oxidation rate (IOR)

The intrinsic oxidation rate (IOR) defines the primary pollutant production rate in a waste rock dump. In column testwork, the IOR can be deduced from the rate of sulphate production as discussed above or directly from the rate of oxygen consumption (Ritchie 1994). In the field, the IOR may be evaluated by analysis of oxygen and temperature profiles, both of which reflect the oxidation rate and gas transport mechanism in the dump. Oxygen and temperature profiles are easily measured with inexpensive instrumentation once an appropriately constructed probe hole has been installed in a waste rock dump. ANSTO has derived simple mathematical models of the IOR to indicate its impact on the time dependence of the overall oxidation in a waste rock dump. Field measurements have been carried out at several mine sites in Australia including Rum Jungle, Norwich Park and Woodlawn (Ritchie 1994) as well as internationally in Sweden, Canada and the United States (Ritchie 1993).

While instrumentation of a waste rock dump can occur at any stage of mine life, implementation at the early stages of mine development is less costly and provides field data at the very early stages of the mine development. As both the parameters of oxygen concentration and temperature are closely related to the pyrite oxidation rate, which is the primary pollutant generation mechanism, they can then be used to provide a direct and rapid indicator of the effectiveness of measures adopted to reduce the oxidation rate in pyritic mine wastes.

Conclusions and recommendations

This study reports on techniques currently used in Australia for assessing the acid mine drainage potential of sulphidic mine wastes. A number of static methods and kinetic methods for determining the pollutant generating potential of sulphidic mine wastes have been reviewed. Due to the limitations inherent with the static testwork methodology, static methods are only satisfactory for the initial screening of mine waste samples into categories of acid consuming, non-acid generating and potentially acid generating—low capacity or high capacity. Column testwork provides time-series data for the measurement of the acid generating characteristics of the waste material and information on leachate quality under controlled laboratory conditions. Such information is valuable for the identification and

evaluation of the geochemical implications of operational placement, long-term storage and management strategies for sulphidic mine wastes.

An assessment of the information received from the OSS/ACMRR survey showed that only 30% of the responding mine sites undertook some form of acid base accounting. Of those, 50% also carried out NAG tests. Less than ten per cent of the responding sites reported having undertaken some form of other test. Most of these sites undertook on-going pH monitoring and/or water quality monitoring or leach column testwork. The latter represents 5% of the responding mine sites. Representative sampling and geological assessment is a critical part of any geochemical assessment program. Of those respondents who specified the number of samples used for ABA tests, almost one-third used less than ten samples for their mine waste characterisation studies. There is no evidence that this number was related to the total amount of waste types generated, but it is unlikely that the number of samples used for the tests were appropriate.

It is apparent from the survey that a protocol is lacking within the Australian mining industry for appropriate sampling of waste samples and the characterisation of mining wastes. It is also evident that existing methodologies for making predictions require identification and validation of the limitations of static and kinetic tests, particularly with respect to site specificity. It is recommended that a protocol is developed such that some standardisation and uniformity is introduced within the Australian mining industry for the characterisation of sulphidic mine wastes. The implementation of predictive models is also encouraged.

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Appendix B Letter from David Buckingham, Executive Director, Minerals Council of Australia (23 May 1996)



23 May, 1996

The Minerals Council of Australia is pleased to support the study by Dr John Harries of the extent of acid drainage at mine sites in Australia.

In a recent examination of environmental exposures for the mining industry, the Council's Environment Committee identified acid drainage as an important area of potential liability and endorsed the value of the proposed study.

It is important that we establish accurate data on the extent and characteristics of acid drainage. Better information will enable better decisions to be made on what action, if any, is needed to mitigate acid drainage problems.

This study is a joint initiative between the minerals industry, other members of the Australian Centre for Minesite Rehabilitation Research and the Office of the Supervising Scientist (part of the Commonwealth EPA). Dr Harries, a Senior Principal Research Scientist with the Environment Division of the Australian Nuclear Science and Technology Organisation, has been appointed as an OSS/ACMRR Fellow specifically for this project.

Data gathered will, for the first time, provide a national picture of the extent of acid drainage at mine sites. The study is being undertaken in close consultation with Chambers of Mines/Minerals Councils and mines departments in all States and the Northern Territory. The cooperation of mining companies and individual operations will ensure the success of the project.

Data gathered on individual sites and companies will be kept confidential. Only aggregate data will be published, unless specific approval for publication of site data has been given by the mine operator. At the completion of the study, raw data will be securely archived by the Minerals Council of Australia on behalf of the ACMRR.

I ask that your company or mining operation cooperates with the study.

If you have any comments or queries about industry involvement in the project, please contact Ian Satchwell at the Minerals Council of Australia on (06) 279 3600. Inquiries regarding technical aspects of the project should be directed to Dr Harries, whose contact details are shown on the survey information sheet.

Yours sincerely

A handwritten signature of David Buckingham.

David Buckingham
EXECUTIVE DIRECTOR

DAB:IDS:DDC

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216 Northbourne Avenue
Canberra ACT 2601
PO Box 361
Dickson ACT 2602
Telephone 06 279 3600
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Appendix C People consulted and organisations visited during OSS/ACMRR study

ARCO Coal Australia, Alex Armstrong

Australian Centre for Minesite Rehabilitation, Clive Bell

Australian Geological Survey Organisation, Canberra, Greg Ewers

Australian Mineral Industries Research Association Ltd (AMIRA), Paul Greenhill

BHP (Coal), Peter Roe (Manager Environmental Services)

BHP (Iron Ore), Ron Hillis (Manager Environmental Services)

Boddington Gold Mine, Craig Moreley (Chief Geologist), Megan James

Brukunga, SA, historic mine site

Bureau Mineral Resources, Brian Elliot, re MINLOC and MINRES databases

Burnside Gold Operations (previously Cosmo Howley), Lloyd Beck

Captains Flat, with Philip West, OSS

Central Queensland Mining Rehabilitation Group, Goonyella/Riverside mine, Moranbah, Qld

Chamber of Mines and Energy of Western Australia Inc, Jane Aberdeen

Collinsville Coal Mine, Paul Stathan (Environmental Officer)

Copper Mines of Tasmania at Queenstown, Isobel Stanley and Alan Robertson

Department of Development and Resources (Tas), Tony Christianson, Ralph Botrell, Bill Baker

Department of Environment and Land Management (Tas), John Johnston (Senior Environmental Management Officer)

Department of Mineral Resources NSW, Dennis Paul Frederickson, Chris Wall, Kerry Brooks, Ken Hollands (Manager Environment)

Department of Minerals and Energy (WA) with Bill Biggs, Hugh Jones and Alan Bradley

Department of Mines and Energy (NT), Tony McGill (Director of Mines), David Lawrence and Barry Noller

Department of Mines and Energy (SA)

Department of Mining and Energy (Queensland), John Bywater and Jaixin Zhou

Department of Energy and Mines (Vic), Tony Wissenden,

Department of Land & Water Management (NSW), Graeme Clifton

Environmental Practice Task Force, Minerals Council of Australia

Environmental Workshop, 3rd International and 21st Annual Environmental Workshop, Australian Minerals Council of Australia, Newcastle, October 1996

ERA Environmental Services, Tony Milne

German Creek Coal Mine, John Merritt (Environmental Officer)

Gordonstone Coal Mine, Cathy Brosnan (Environmental Officer)

Hamersley Iron Ore Pty Ltd with Jim Stoddart (Manager Environmental Affairs)

John Anderson, consultant

Kalgoorlie Consolidated Gold Mines (KCGM), Gay Bradley (Senior Rehabilitation Officer),
Gary Lye, (Geotechnical Superintendent), Bruce McFadzean, (Open Pit Superintendent)

Kaltails Project (Kalgoorlie Tailings Retreatment Project), Greg Barrett

Kwinana Nickel Refinery, WMC Resources, Les Cousins (Environmental Scientist)

MIM, David Hughes (MIM Manager Environmental Affairs)

Minerals Council of Australia, David Buckingham, Ian Satchwell

Mount Leyshon Gold Mines, Paul Veivers (Environmental Officer)

Mount Tom Price, Hamersley Iron Ore: Ken Ramsey (Environmental Superintendent)

Mt Lyell Rehabilitation Project

North Limited, Peter McNally

Northparkes Mine (NSW), Andrew Reid

NSW Chamber of Mines, Newcastle, John Hannan (Environment Manager)

NT Chamber of Mines, Ms Kezia Purick (Chief Executive Officer)

Office of the Supervising Scientist, Darwin, Peter Waggett, Peter Bailey

Office of the Supervising Scientist, Canberra, Stewart Needham, Patrick McBride, Philip West

Pajingo Gold Mine (meeting in Charters Towers), Ian Tredinnick (Superintendent Technical Services)

Parks and Wildlife Commission of NT, Rod Applegate,

Peak Hill Mine (NSW), Michael Sutherland

Pine Creek (RGC) Gold Mine, Mike Fawcett, Chris Wilson

Placer Pacific, Sydney, Gavin Murray

Queensland Mining Council, Environment Committee

Ravenswood Gold Mines, Rob Hunt (Environmental Coordinator)

RGC Thalanga Mine, Jim Taylor (Environmental Officer)

RGC Perth, Dennis Brookes

Rum Jungle mine site

Tasmania Acid Drainage Working Group Meeting, Queenstown, Tas

Union Mining, Christine Brown

Union Reefs Mine, Cameron Switzer (Senior Geologist)

Victorian Chamber of Mines, John Reynolds

Western Mining Company (Perth) Michael Anstey (Senior Environmental Advisor—Gold)

Western Mining Company, George White (Group Environmental Advisor)

Woodlawn Mine, Roger Jackman,

2nd National Acid Sulphate Soils Conference, Coffs Harbour

I am very grateful for the wide ranging discussions with the people listed and also the many others I have spoken to by phone and at various meetings.

John Harries

Appendix D Questionnaire form distributed to mine sites

CONFIDENTIAL

Minesite ID Number: «MineNo»

ACMRR/OSS Acid Mine/Rock Drainage Study Current Mining Leases

1. Mine Number	«MineNo»
2. Mine Name	«Minesite»
3. Mineral Type	
4. Contact Person	
5. Address	
6. Phone	
7. Fax	

The information provided will be used to develop the aggregated data to be used in the ACMRR/OSS study of extent of acid mine drainage and acid rock drainage in the Australian mining industry and the associated liability. Information on these sheets will be treated as confidential.

I would be grateful if you could provide means and ranges and indicate the relative proportions if there is a large range of values. Please use additional sheets if more space is needed or provide copies of printed data or strategies if available.

If you have any queries about the information requested, need any clarification, find the categories do not adequately apply to your operation, please contact John Harries on 02 9717 3896 (work), 02 9520 7562 (home), 02 9717 9260 (fax) or jrh@ansto.gov.au (email).

Please return the completed form to John Harries at ANSTO Environment Division, PMB 1, Menai, NSW 2234 or the fax number above by 25 September 1996.

ACMRR/OSS Acid Mine/Rock Drainage Study

CONFIDENTIAL		Minesite ID Number: «MineNo»	
8.	Is surface water released from lease treated?	Y/N	23. Have any acid-base accounting measurements been carried out?
9.	Type of water treatment?		24. If so what sort and how many?
10.	Annual flow M ³ /y?		25. Any other prediction measurements e.g. leach columns?
11.	Ground water:	Fresh (<1500 mg/L TDS), Brackish (1500-5000 mg/L TDS) Saline (5,000-15,000 mg/L TDS) Very Saline (>15,000 mg/L TDS)	26. Comments e.g. Special site conditions/requirements Proposals to manage AMD/ARD at mine closure Strategic significance of AMD/ARD at this mine
12.	Is ground water quality monitored		
13.	Opencuts:	Y/N	
14.	Is seepage water pumped?	Y/N	
15.	Pumping rate?		
16.	Water quality?		
17.	Any water filled opencuts/voids?	Y/N	
18.	How much water contained (m ³)?		
19.	Water quality?		
20.	Any underground workings/adits?		
21.	Is there seepage water?		
22.	How much?		
	Water quality?		

CONFIDENTIAL

Please provide information on mine wastes/residues/stockpiles that contain or might contain potentially acid generating material.

WASTE ROCK/OVERBURDEN/COAL REJECT /CO-DISPOSAL		TAILINGS (Process Residues)		STOCKPILES (low-grade/mineralised)	
		HEAP LEACH RESIDUES			
27. Sections or name of dump/dam					
28. Weight (Mt)					
29. Volume (Mm ³)					
30. Area (ha)					
31. Total Sulfur (%) principal sulfides sulfides % sulfates % organic sulfur %					
32. Pyrite/pyrrhotite Content (%), what distribution					
33. Carbonate % what minerals					
34. Results of Acid/Base accounting measurements on waste (NAPP, NAG, etc)					
35. Typical pH of seepage from waste					
36. Long term management strategy					

Appendix E List of the mine sites included in the survey

Minesite	Type	Minesite	Type
Agnew Gold Operations	Au	Bronzewing Gold Mine	Au
Anglesea Coal Mine	Coal	Browns Creek Mine	Au/Cu
Angus Place Colliery	Coal	Brunswick Mine	Au/Sb
Appin Colliery	Coal	Bulga Open Cut	Coal
Argyle Diamond Mine	Diamond	Burbanks	Au
Aroona & Beltana Mines	Ag/Pb/Zn	Burgowan No 12 Underground	Coal
Avoca Alluvial Gold Project	Au	Cadjeput & Goongewa Mine	Pb/Zn
Awaba Colliery	Coal	Callide Mine	Coal
Baalbone Colliery	Coal	Camberwell Coal Mine	Coal
Bailieston	Au	Camel Creek–Golden Cup	Au
Balcooma Project	Zn/Cu	Canyon Colliery	Coal
Ballarat East Gold Project	Au	Capel Mine	Mineral sands
Ballarat Gold Project	Au	Century Mine	Zn
Bamboo Creek Mine	Au	Chain Valley Colliery	Coal
Bardoc Davyhurst Joint Venture	Au	Chalice	Au
Bayleys/Lindays Mine	Au	Channar	Iron ore
Bayswater No 2 Open Cut	Coal	Charbon Colliery	Coal
Beaconsfield Mine	Au	Chicken Creek Open Cut	Coal
Beenup Mine	Mineral sands	Clarence Colliery	Coal
Bellevue Gold Project	Au	Cobar Csa Mine	Cu/Ag/Pb/Zn
Benambra Mine	Base metal	Collinsville Coal Company	Coal
Berrima Colliery	Coal	Cook Colliery	Coal
Big Bell Mine	Au	Copperhead/Golden Pig Mine	Au
Big Rush	Au	Cordeaux Colliery	Coal
Biggenden	Magnetite	Cosmo Howley/Burnside Operations	Au
Binduli Gold Mine	Au	Cracow Gold Mine	Au
Blackwater Mine	Coal	Croydon	Au
Blackwood & Duncan Coal Mine	Coal	Crinum Mine	Coal
Blair Athol Coal Project	Coal	Cumnock No 1 Colliery	Coal
Bloomfield Mine	Coal	Curragh Mine	Coal
Blue Bar	Au	Darlot Mine	Au
Blue Mountains Colliery	Coal	Dartbrook	Coal
Blue Spec–Golden Spec Mine	Au	Drayton Coal Mine	Coal
Bluebird Gold Mine	Au	Eloise	Cu/Au/Ag
Boddington Gold Mine	Au	Elouera Colliery	Coal
Boundary Hill Mine	Coal	Elura Mine	Ag/Pb/Zn
Bounty Gold Mine	Au	Emmaville Tin Mine	Sn
Bow River Diamond Mine	Diamond	Endeavour Colliery	Coal
Brimstone Colliery	Coal	Eneabba Operations	Mineral sands
Brockman No 2 Detrital	Iron Ore	Ensham Mine	Coal
Brocks Creek	Au	Ernest Henry Project	Cu

Minesite	Type	Minesite	Type
Ewington 2	Coal	Invincible Colliery	Coal
Fimiston Mine/Super Pit	Au	Iron Duke	Iron ore
Forrestania Nickel	Ni	Iron Knob	Iron ore
Fortescue	Iron ore	Ivanhoe Colliery	Coal
Fortnum Gold Mine	Au	Jangardup, Busselton & Waroona	Mineral sands
Fosterville Gold Project	Au	Jeebropilly	Coal
Fraser Gold Mine (incl Golden Pig)	Au	Jellinbah Central Mine	Coal
Gaffney's Creek Goldmine Ni	Au	Jimblebar Iron Ore	Iron ore
Gecko Copper/Gold Mine	Au/Cu	Jubilee Gold Mine	Au
Georgetown Mine	Au	Jundee Gold Mine	Au
German Creek Mine O/Cut	Coal	Kaltails Project	Au
Gidgee Gold Mine	Au	Kambalda Nickel Mine	Ni
Girilambone Copper Mine	Cu	Kandos No 3 Colliery	Coal
Golden Crown	Au	Kanowna Belle Mine	Au
Golden Web	Au	Kara Mine	Magnetite
Goodall	Au	Kidston Mine	Au
Goonyella/Riverside Mine	Coal	Kookynie Project	Au
Gordonstone Coal Mine	Coal	Koolyanobbing Iron Ore Project	Iron Ore
Granny Smith	Au	Kundana Mine	Au
Great Australia Copper Mine	Cu	Kurildala	Cu
Great Greta Colliery	Coal	Lady Bountiful Extended Mine	Au
Great Lady Gold Mine	Au	Lanfranchi/Schmitz	Ni
Greenbushes Mine	Pegmatite	Laverton Mine	Au
Greenfields Mine	Au	Lawlers Gold Mine	Au
Gregory Mine Joint Venture	Coal	Leichhardt Creek Tin Mine	Sn
Gretley Colliery	Coal	Leigh Creek Coalfield	Coal
Gullewa	Au	Leinster Nickel Operations	Ni
Gunnedah Colliery	Coal	Lemington Mine	Coal
Gunpowder Mine	Cu	Liddell Colliery	Coal
Gympie Mine	Au	Lower Bielsdown Antimony Proj	Sb
Harbour Lights Mining Limited	Au	Loy Yang Mine	Coal
Hawks Nest Mine	Mineral sands	Lynas Find	Au
Hazelwood Mine	Coal	M.W. Haenke No. 2 Underground	Coal
Hedges Gold	Au	Maddingley Brown Coal Co	Coal
Hellyer Mine	Ag/Pb/Zn	Manumbar	Au
Henty Gold Project	Au	Marandoo	Iron ore
Hill 50 Gold Mine Ni	Au	Mariners Kambalda Nickel	Ni
Hillgrove Gold-Antimony Mine	Au/Sb/As	Marvel Loch Mine	Au
Hilton Mine	Ag/Pb/Zn	Marymia	Au
Holleton	Au	McArthur River	Ag/Pb/Zn
Howick Open Cut	Coal	McKinnons Mine	Au
Hunter Valley Coal Mines	Coal	Meandu Mine (Tarong Coal)	Coal

Minesite	Type	Minesite	Type
Meekatharra Gold Mine	Au	Norris Mine	Au
Merrywood	Coal	Norseman Operations	Au
Metropolitan Collieries	Coal	North Goonyella Mine	Coal
Mineral Hill	Au/Cu	North Stradbroke Island	Mineral sands
Moonee	Coal	Northparkes Mines	Au/Cu
Mount Coolon	Au	Norwich Park Mine	Coal
Mount Gibson	Au	Oakdale Colliery	Coal
Mount Gunson	Cu	Oaky Creek Mine	Coal
Mount Hogan	Au/Ag	Olympic Dam Operations	Cu/U/Au/Ag
Mount Isa Mine	Pb/Zn/Cu/Ag	Ora Banda	Au
Mount Rankin Mine	Au	Orebody 18	Iron ore
Mount Thorley Mine	Coal	Orient Well	Au
Moura Mine	Coal	Orlando Project	Au
Mt Charlotte Mine	Au	Osborne Mines	Au/Cu
Mt Keith Nickel Operation	Ni	Paddington Mine	Au
Mt Leyshon Mine	Au	Pajingo Gold Mine	Au
Mt Lyell Mine	Cu/Au	Palm Springs	Au
Mt McClure Gold Mine	Au	Pan West Tantalum	Tantalum
Mt Monger Gold Operations	Au	Pannawonica-Deepdale	Iron ore
Mt Monger Joint Venture	Au	Paraburadoo Mine	Iron ore
Mt Morgans Mine	Au	Parkes Gold Project/Calerie	Au
Mt Percy Mine	Au	Pasminco Mining – Broken Hill	Ag/Pb/Zn
Mt Todd Mine	Au	Peak Downs Mine	Coal
Mt Tom Price	Iron Ore	Peak Hill (NSW)	Au
Mt Whale Back Mine	Iron Ore	Peak Hill (WA)	Au
Muja Open Cut	Coal	Pine Creek	Au/Ag
Mulline	Au	Plutonic Gold Mine (Inc Freshwater)	Au
Munmorah Colliery	Coal	Poseidon South	Au
Muswellbrook No 2 Open Cut	Coal	Potosi Mine	Ag/Pb/Zn
Muswellbrook No 2 Underground	Coal	Preston Extended Mine	Coal
Myuna Colliery	Coal	Quamby Gold Mine	Au
Narngulu Operations	Mineral Sands	Ranger Mine	U
Narran Vale Mine	Sapphire	Ravensworth/Narama Mine	Coal
Nevoria Gold Mine	Au	Red Dome Gold Mine	Au/Cu/Ag
New Celebration Mine	Au	Red, White And Blue	Au
New Hope Collieries	Coal	Redbank Mine	Cu
Newhill Underground Mine	Coal	Reddestone Creek No. 1 & 2	Sapphire
Newlands Coal Mine	Coal	Reedy Gold Mine	Au
Newstan Colliery	Coal	Renison Tin Mine	Sn
Nifty Mine	Au	Rishton	Au
Nimringarra	Iron Ore	Riverina	Au
Nolans Gold Mine	Au	Rixs Creek Mine	Coal

Minesite	Type	Minesite	Type
Rosebery Mine	Pb/Zn/Cu/Au/Ag	Viney Creek	Mineral sands
Rustlers Roost Gold Mine	Au	Wallarah Colliery	Coal
Sandstone (Elmina)	Au	Wambo Colliery	Coal
Sandstone Mine	Au	Wannaway	Ni
Saraji Mine	Coal	Warkworth Mine	Coal
Savage River Mines	Iron ore	Wattle Glen Open Cut	Coal
Scuddles Zinc Mine	Zn	Wattle Gully Gold Mine	Au
Selwyn Gold Mine	Au/Cu	West Cliff Colliery	Coal
Shamrock Mine	Au	West Wallsend Colliery	Coal
Sons Of Gwalia Mine	Au	Western Collieries Ltd	Coal
South Blackwater Coal Mine	Coal	Westside Mine	Coal
South Bulga Colliery	Coal	White Devil Mine	Au
South Bulli Colliery	Coal	Whiteheads Project	Au
South Walker Creek	Coal	Wilkie Creek Coal Project	Coal
Springvale Colliery	Coal	Wiluna Gold	Au
St Arnaud	Au	Windarra Nickel Project	Ni
St Ives Gold Mines	Au	Windimurra Vanadium Mine	Vanadium
Stawell Gold Mine	Au	Woodcutters Mine	Base metal
Stratford Coal Mine	Coal	Woolawn Mine	Pb/Cu/Zn
Strathdarr Mine	Sapphire	Wyee Colliery	Coal
Tahmoor Colliery	Coal	Yallourn Mine (SECV)	Coal
Tallawang Magnetite Mine	Magnetite	Yandan Gold Mine	Au
Tanami (Central Desert J.V.)	Au	Yarrabee Mine	Coal
Tarmoola Mine	Au	Yarrie Mine	Iron ore
Telfer Gold Mine	Au	Yilgarn Star Project	Au
Ternora Mine	Au	Yoganup North/Yoganup Extended	Mineral sands
Teralba Colliery	Coal	Youanmi Gold Mine	Au
Thalanga Mine	Base metal		
The Granites Gold Mine	Au		
The Peak Mine	Base metal		
Thiel Well Gold Operation	Au		
Three Mile Hill Project	Au		
Tick Hill	Au		
Tiwest Joint Venture	Mineral sands		
Tomago Mine	Mineral sands		
Tower Colliery	Coal		
Tuckabianna Gold Mine	Au		
Two Boys Gold Mine	Au		
Ulan Coal Mine	Coal		
Union Reefs Gold Mine	Au		
United Collieries Pty Ltd	Coal		
Vickery Mine	Coal		